## ABSTRACT

This program designs rectangular steel base plates supporting eccentrically loaded steel columns in accordance with the seventh edition of the AISC Specification (1969) and the ACI Building code. Price $\$ 60.00$

## INPUT

Number and size of bolts
Plate dimensions
Allowable bending stress
Concrete compressive strength Axial load
Applied moment

## OUTPUT

Eccentricity of load
Length of soil pressure diagram
Tensile force per bolt
Tensile stress per bolt
Maximum bearing stress
Allowable bearing stress
Required plate thickness

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## Data: C. P. 120

| Size of bolts ( $\phi$ ) | = | 1.5 | in. |
| :---: | :---: | :---: | :---: |
| Number of bolts on tension side (NB) | = | 2 | bolts |
| Length of plate (D) | = | 34.75 | in. |
| Distance from center of bolts to plate edge (E) | = | 2.5 | in. |
| Width of plate (B) | = | 17 | in. |
| Axial load (Pc) | = | 300 | kips |
| Allowable steel bending stress for plate ( $\mathrm{f}_{\mathrm{S}}$ ) | = | 27 | ksi |
| Compressive strength of concrete ( $\mathrm{f}^{\prime} \mathrm{c}$ ) | $=$ | 3 | ksi |
| Applied moment (M) | = | 500 | k - ft |

## Calculations:

| Eccentricity of load; $e=12 \mathrm{M} / \mathrm{P}$ | = | 20.0000 | in. |
| :---: | :---: | :---: | :---: |
| Three roots of cubic equation Rl |  |  |  |
| R2 |  | 0.0000 |  |
| R3 | = | 16.0452 |  |
| Length of soil pressure diagram (Y) | $=$ | 16.0452 | in. |
| Tension force per bolt; $\mathrm{F}_{2}=\mathrm{Pt} / \mathrm{NB}$ | = | 44.4586 | kips |
| Bolt stress; $\mathrm{fa}=4 \mathrm{~F} / \pi \phi^{2}$ | = | 25.1584 | ksi |
| Maximum bearing stress in concrete (fbm) | = | 2.8516 | ksi |
| Allowable bearing stress: $\mathrm{fb}=.375 \mathrm{f}$ ' c | = | 1.1250 | ksi |
| Width of column (b) | $=$ | 10 | in. |
| Depth of column (d) | = | 15 | in. |
| Bolt eccentricity in $Y$ direction ( h ) | = | 3 | in. |
| Plate moment; $\mathrm{M}_{\mathrm{X}}=\mathrm{Pt}((\mathrm{D}-\mathrm{d}) / 2-\mathrm{E})$ | = | 655.7650 | $k$ - in. |
| Thickness $=\sqrt{6 \mathrm{M}_{\mathrm{X}} / \mathrm{Bf}_{s}}$ | = | 2.9277 | in. |
| Plate moment; $\mathrm{My}^{\text {y }}=\mathrm{F}(\mathrm{h})$ | = | 133.3758 | k-in. |
| Thickness $=\sqrt{6 \mathrm{My} /(\mathrm{E}+\mathrm{G}) \mathrm{f}_{\mathrm{s}}}$ | = | 1.7324 | in. |
| Plate moment; $\mathrm{Mxx}^{\text {a }}$ f $\mathrm{fbm}(\mathrm{B})(\mathrm{m})^{2} / 2$ | = | 2546.5679 | k-in. |
| Thickness $=\sqrt{6 \mathrm{M}_{\mathrm{Xx}} / \mathrm{Bfs}}$ | = | 5.7696 | in. |
| Plate moment; ${ }^{\text {Myy }}=\mathrm{fbm}(\mathrm{E}+\mathrm{G}) \mathrm{n} 2 / 2$ | = | 285.1148 | k-in. |
| Thickness $=\sqrt{6 \mathrm{Myy}^{\prime} /(\mathrm{E}+\mathrm{G}) \mathrm{f}_{s}}$ | = | 2.5329 | in. |

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