

#3 TEE SECTION PROPERTIES

ABSTRACT

This program computes the precast and composite section properties for double tees and single tees with or without sloping webs. Flanges must be uniform in thickness. Transformed section properties can also be computed if steel is to be considered.

Price \$60.00

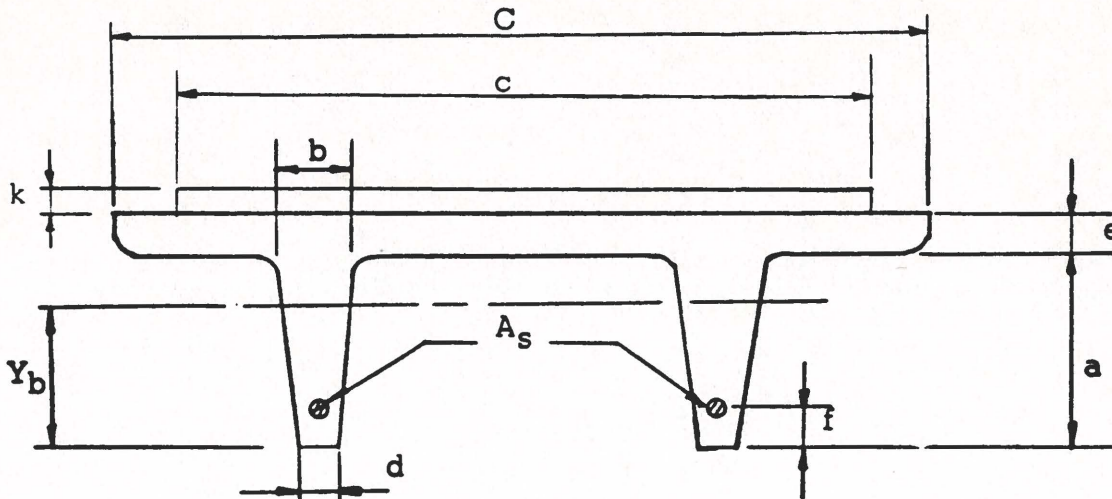
INPUT

Dimensions of tee  
Elasticity of steel and concrete  
Area and location of steel  
Transformed topping width

OUTPUT

Centroid for top and bottom  
Moment of inertia  
Section modulus for top and bottom  
Area

SECTION PROPERTIES



C.P. - 3

**Data:**

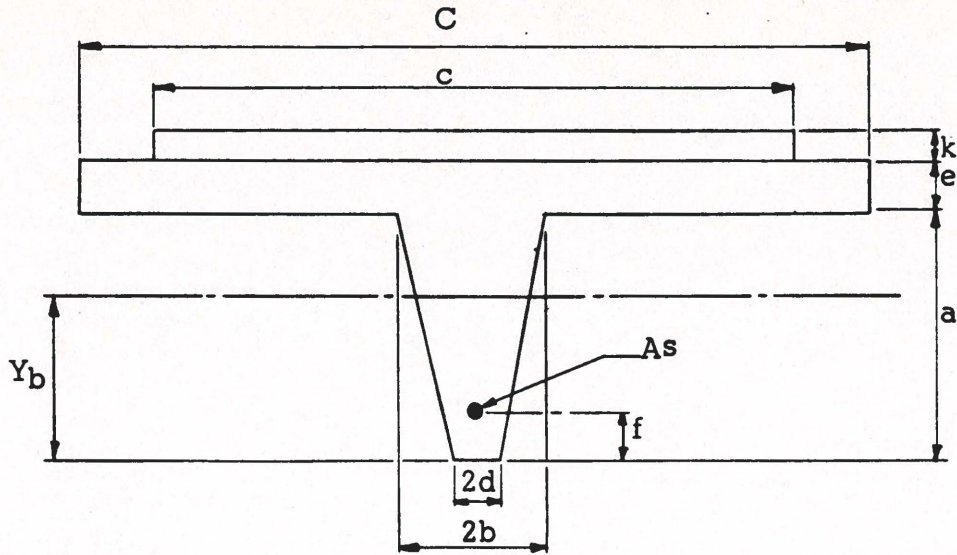
Depth of stem (a)	=	28	in.
Width of stem (b)	=	6	in.
Width of flange (c)	=	96	in.
Width of stem (d)	=	3.25	in.
Modulus of Elasticity of steel ( $E_s$ )	=	30000	ksi.
Modulus of Elasticity of concrete ( $E_c$ )	=	3000	ksi.
Area of Steel reinforcement ( $A_s$ )	=	3.0	in. <sup>2</sup>
Flange Thickness (e)	=	4	in.
Center of gravity of steel (f)	=	2	in.

**Calculations:**

Distance from bottom to neutral axis ( $Y_b$ )	=	23.1282	in.
Moment of Inertia (I)	=	63979.2773	in. <sup>4</sup>
Section Modulus -- bottom ( $S_b$ )	=	2766.2886	in. <sup>3</sup>
Distance from top to neutral axis ( $Y_t$ )	=	6.8716	in.
Area (.A)	=	673.0000	in. <sup>2</sup>
Section Modulus -- Top $S_t$	=	7211.5328	in. <sup>3</sup>
Thickness of topping (k)	=	3	in.
Transformed width of topping (C)	=	60	in.
Area of composite section ( $A_t$ )	=	853.0000	in. <sup>2</sup>
Centroid of composite section ( $Y_b$ )	=	25.3168	in.
Centroid of composite section ( $Y_t$ )	=	9.6832	in.
Inertia of composite section ( $I_t$ )	=	79391.5260	in. <sup>4</sup>
Section modulus wrt. bottom ( $S_b$ )	=	3135.9226	in. <sup>3</sup>
Section modulus wrt. top ( $S_t$ )	=	8198.8935	in. <sup>3</sup>



SECTION PROPERTIES



C.P. - 3

**Data:**

Depth of stem (a)	=	20 in.
Width of stem (b)	=	5 in.
Width of flange (c)	=	90 in.
Width of stem (d)	=	2 in.
Modulus of Elasticity of steel ( $E_s$ )	=	29000 ksi.
Modulus of Elasticity of concrete ( $E_c$ )	=	4000 ksi.
Area of Steel reinforcement ( $A_s$ )	=	2 in. <sup>2</sup>
Flange Thickness (e)	=	3 in.
Center of gravity of steel (f)	=	2 in.

**Calculations:**

Distance from bottom to neutral axis ( $Y_b$ )	=	17.2091 in.
Moment of Inertia (I)	=	17011.9200 in. <sup>4</sup>
Section Modulus -- bottom ( $S_b$ )	=	988.5421 in. <sup>3</sup>
Distance from top to neutral axis ( $Y_t$ )	=	5.7909 in.
Area (.A)	=	394.5000 in. <sup>2</sup>
Section Modulus -- Top $S_t$	=	2937.6988 in. <sup>3</sup>
Thickness of topping (k)	=	2 in.
Transformed width of topping (C)	=	65 in.
Area of composite section ( $A_t$ )	=	524.5000 in. <sup>2</sup>
Centroid of composite section ( $Y_b$ )	=	18.9922 in.
Centroid of composite section ( $Y_t$ )	=	6.1078 in.
Inertia of composite section ( $I_t$ )	=	21564.4409 in. <sup>4</sup>
Section modulus wrt. bottom ( $S_b$ )	=	1141.4467 in. <sup>3</sup>
Section modulus wrt. top ( $S_t$ )	=	3530.6396 in. <sup>3</sup>

## #7 FIXED END MOMENTS AND REACTIONS

### ABSTRACT

This program computes fixed end moments and reaction for beams with any number and/or combination of loads such as point loads, triangular loads, uniform loads, and applied moments. Triangular and uniform loads may be partially or fully distributed on the beam. End joints can be pinned or fixed on either end or on both ends.

Price        \$60.00

### INPUT

Load description  
Joint type  
Span length

### OUTPUT

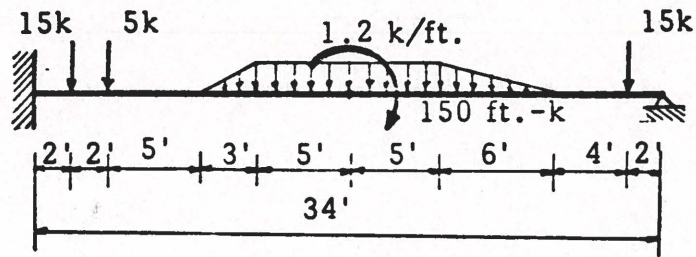
Left moment  
Right moment  
Left reaction  
Right reaction



C. P. 7

SAMPLE PROBLEM

Given:



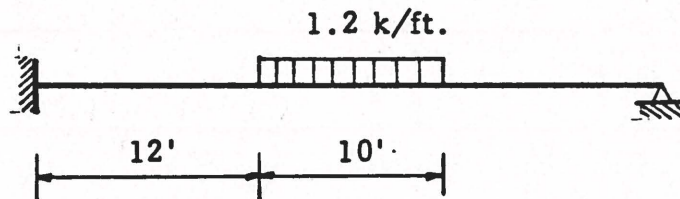
$$J_a = 1$$

$$J_b = 0$$

$$\text{Span Length } L = 34 \text{ ft.}$$

Solution: The beam must be broken down into the following five loadings.

Loading 1



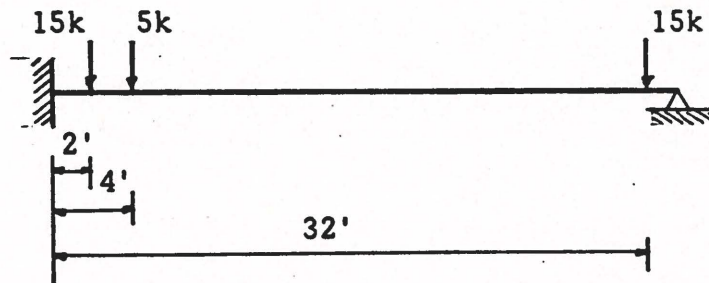
Type of Loading = 1

$W = 1.2 \text{ k/ft.}$

$A = 12 \text{ ft.}$

$B = 10 \text{ ft.}$

Loading 2



Type of Loading = 2

Number of Loads,  $N = 3$

$P(1) = 15 \text{ k}$

$A(1) = 2 \text{ ft.}$

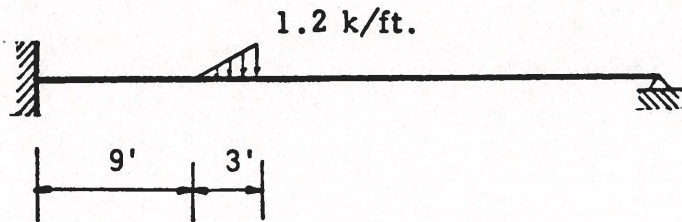
$P(2) = 5 \text{ k}$

$A(2) = 4 \text{ ft.}$

$P(3) = 15 \text{ k}$

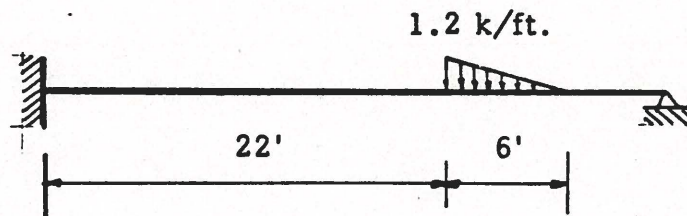
$A(3) = 32 \text{ ft.}$

Loading 3



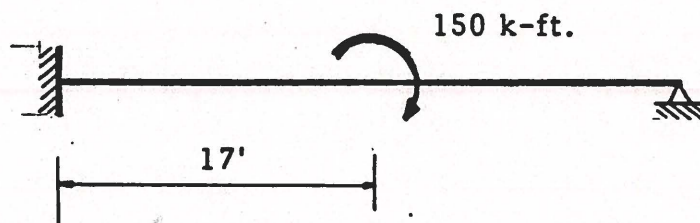
Type of Loading = 3  
W = 1.2 k/ft.  
S = +1  
A = 9 ft.  
B = 3 ft.

Loading 4



Type of Loading = 3  
W = 1.2 k/ft.  
S = -1  
A = 22 ft.  
B = 6 ft.

Loading 5



Type of Loading = 4  
Mo = 150 k-ft.  
A(1) = 17'



Data:

Left Joint Type, Ja	1	S
Right Joint Type, Jb	0	S
Span Length, L	34	S
<u>Loading 1</u> , Type of Loading	1	S
Applied Uniform Load, W	1.2	S
Distance from Left Support, A	12	S
Distance Load is Applied, B	10	S
Left Reaction, Ra	8.1852	e0
Right Reaction, Rb	3.8148	E0
Left Moment, Ma	-74.2941	f0
Right Moment, Mb	0.0000	F0
<u>Loading 2</u> , Type of Loading	2	S
Number of Loads, N	3	S
P(1)	15	S
A(1)	2	S
P(2)	5	S
A(2)	4	S
P(3)	15	S
A(3)	32	S
Summation of Ra, Loading 1 and 2	29.3294	e0
Summation of Rb, Loading 1 and 2	17.6706	E0
Summation of Ma, Loading 1 and 2	-133.2558	f0
Summation of Mb, Loading 1 and 2	0.0000	F0
<u>Loading 3</u> , Type of Loading	3	S
Maximum Value of Triangular Load, W	1.2	S
Slope of Triangular Load	1	S
Distance from Left Support, A	9	S
Distance Load Is Applied, B	3	S
Summation of Ra, Loading 1, 2 and 3	30.8764	e0
Summation of Rb, Loading 1, 2 and 3	17.9236	E0
Summation of Ma, Loading 1, 2 and 3	-144.4538	f0
Summation of Mb, Loading 1, 2 and 3	0.0000	F0
<u>Loading 4</u> , Type of Loading	3	S
Maximum Value of Triangular Load, W	1.2	S
Slope of Triangular Load	-1	S
Distance from Left Support, A	22	S
Distance Loas Is Applied, B	6	S
Summation of Ra, Loading 1, 2, 3 and 4	32.4162	e0
Summation of Rb, Loading 1, 2, 3 and 4	19.9838	E0
Summation of Ma, Loading 1, 2, 3 and 4	-160.8070	f0
Summation of Mb, Loading 1, 2, 3 and 4	0.0000	F0
<u>Loading 5</u> , Type of Loading	4	S
Applied Moment, Mo	150	S
Distance from Left Support, A(1)	17	S
Summation of Ra, Loading 1, 2, 3, 4 and 5	27.4530	e0
Summation of Rb, Loading 1, 2, 3, 4 and 5	24.9470	E0
Summation of Ma, Loading 1, 2, 3, 4 and 5	-142.0570	f0
Summation of Mb, Loading 1, 2, 3, 4 and 5	0.0000	F0

**Conclusions:**

**Left Reaction,  $R_a = 27.45$  kips**

**Right Reaction,  $R_b = 24.95$  kips**

**Left Moment,  $M_a = -142.06$  k-ft.**

**Right Moment,  $M_b = 0$**



#10 BEAM DEFLECTION ANALYSIS

**ABSTRACT**

This program computes the deflection at any point X along the span due to applied end moments, uniform load, and any number of point loads. Deflection due to each load type plus total deflection is output.

Price \$65.00

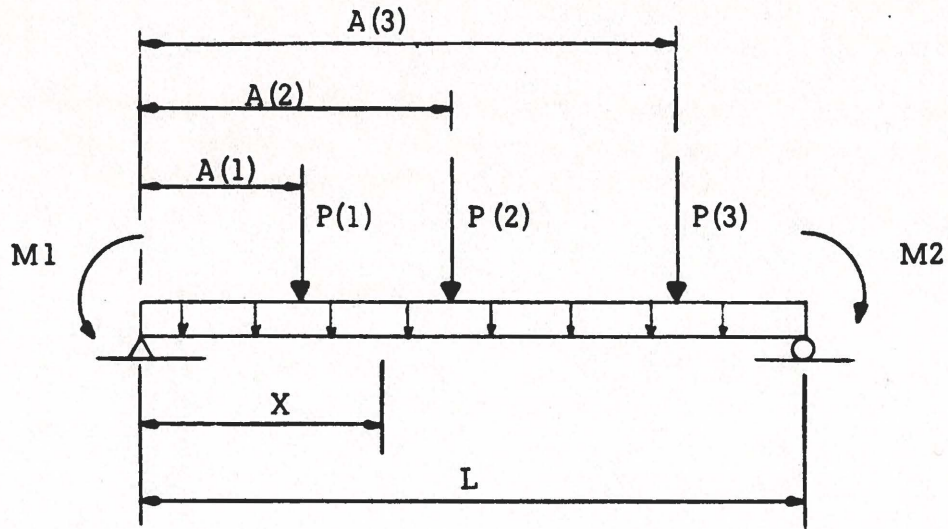
**INPUT**

Span length  
Elasticity and inertia  
Location of desired deflection - X  
End moments  
Uniform and point loads

**OUTPUT**

Deflection due to uniform load  
Deflection due to end moments  
Deflection due to each point load  
Total deflection at X

DEFLECTION ANALYSIS



C.P. 10

Data:

Span length (L)	=	40	ft.
Modulus of elasticity (E)	=	30000	ksi.
Moment of inertia (I)	=	705	in. <sup>4</sup>
Location of desired deflection (X)	=	15	ft.
Moment at left end (M1)	=	200	k-ft.
Moment at right end (M2)	=	150	k-ft.
Uniform load on span (W)	=	0.6	k/ft.

Calculations:

$D_w = 72(W)X(L^3 - 2L(X)^2 + X^3)/E(I)$	=	1.5127	in.
$D_m = \frac{288(X-L)X}{E(I)L} [L(2M1+M2) + X(M2-M1)]$	=	-2.7127	in.
Location of load P(1)	=	10	ft.
Load P(1)	=	25	kips
Deflection at X due to P(1)	=	1.8617	in.
Total deflection at X	=	0.6617	in.
Location of load P(2)	=	25	ft.
Load P(2)	=	26	kips
Deflection at X due to P(2)	=	2.2902	in.
Total deflection at X	=	2.9519	in.

etc.



#22 SECTION PROPERTIES

**ABSTRACT**

This program computes the section properties for any shape that can be represented by rectangles, triangles, circles, and rolled sections. Circles may be subtracted or added from the shape. Listed below are some of the sections the program will solve. Price \$75.00

Single and double tees  
ASSHO girders  
Hollowcore slabs  
Rolled sections with plates added  
Section built up out of plates  
Combination of rolled sections with plates

**INPUT**

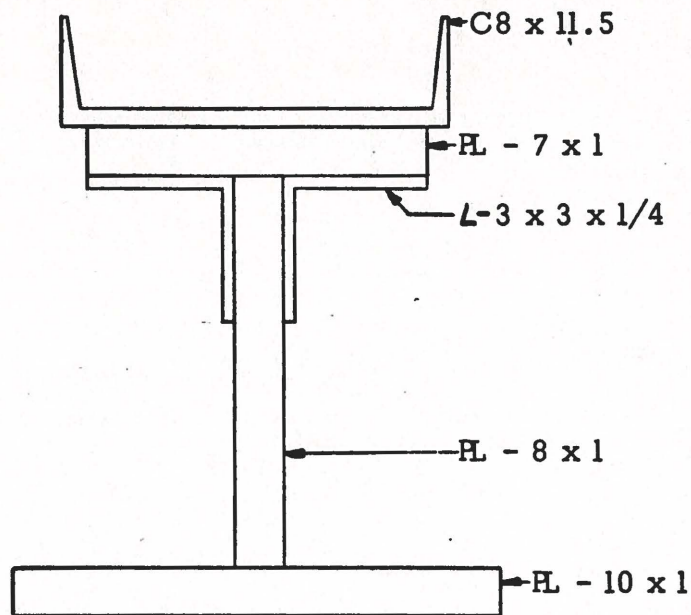
Element type  
Element dimensions

**OUTPUT**

Area  
Centroid with respect to top and bottom  
Moment of inertia  
Radius of gyration  
Section modulus with respect to top and bottom

SAMPLE PROBLEM - CP 22

Given:



Conclusions:

Area of section (A)	=	31.2600	in. <sup>2</sup>
Centroid of section wrt. base ( $Y_b$ )	=	5.4613	in. <sup>4</sup>
Moment of inertia of section (I)	=	519.0743	in. <sup>3</sup>
Section modulus wrt. base ( $S_b$ )	=	95.0459	in. <sup>3</sup>
Radius of gyration (r)	=	4.0749	in.
Section modulus wrt. top ( $S_t$ )	=	76.4615	in. <sup>3</sup>
Centroid of section wrt. top ( $Y_t$ )	=	6.7887	in.



SECTION PROPERTIES

Data: C.P. 22

Number of rectangles (NR)	=	3
Number of rolled shapes (NRO)	=	2
Number of triangles (NT)	=	0
Number of circles (NC)	=	0
Width of rectangle 1 (B1)	=	10 in.
Depth of rectangle 1 (D1)	=	1 in.
Distance to centroid rectangle 1 (Y1)	=	0.5 in.
Width of rectangle 2 (B2)	=	1.0 in.
Depth of rectangle 2 (D2)	=	3 in.
Distance to centroid rectangle 2 (Y2)	=	5 in.
.		
Width of rectangle NR ( $B_{NR}$ )	=	7 in.
Depth of rectangle NR ( $D_{NR}$ )	=	1 in.
Distance to centroid rectangle NR	=	9.5 in.
.		
Area of rolled shape 1 (A1)	=	3.38 in. <sup>2</sup>
Distance to centroid of shape 1 (Y1)	=	10.57 in. <sup>4</sup>
Inertia of shape 1 about its centroid (I1)	=	1.32 in. <sup>4</sup>
.		
Area of rolled shape N (AN)	=	2.38 in. <sup>2</sup>
Distance to centroid of shape N (YN)	=	8.158 in. <sup>4</sup>
Inertia of shape N about its centroid (IN)	=	2.49 in. <sup>4</sup>
.		
Width of triangle 1 (B1)	=	in.
Depth of triangle 1 (D1)	=	in.
Distance to centroid of triangle 1 (Y1)	=	in.
.		
Width of triangle NT	=	in.
Depth of triangle NT	=	in.
Distance to centroid of triangle NT	=	in.

Radius of circle 1	=	in.
Distance to centroid of circle 1	=	in.
Radius of circle 2	=	in.
Distance to centroid of circle 2	=	in.

Radius of circle NC	=	in.
Distance to centroid of circle NC	=	in.

Computations;

Area of section (A)	=	31.2600 in. <sup>2</sup>
Centroid of section wrt. base ( $Y_b$ )	=	5.4613 in.
Moment of inertia of section (I)	=	519.0743 in. <sup>4</sup>
Section modulus wrt. base ( $S_b$ )	=	95.0159 in. <sup>3</sup>
Radius of gyration (r)	=	4.0719 in.
Total depth of section (d)	=	12.25 in.
Section modulus wrt. top ( $S_t$ )	=	76.4615 in. <sup>3</sup>
Centroid of section wrt. top ( $Y_t$ )	=	6.7887 in.



#25 BEAM ANALYSIS

ABSTRACT

This program computes the reactions and then the shear and moment at any number of locations along the beam due to point loads, uniform load and end moments. Maximum positive moment and points of inflection are easily obtained.

Price \$60.00

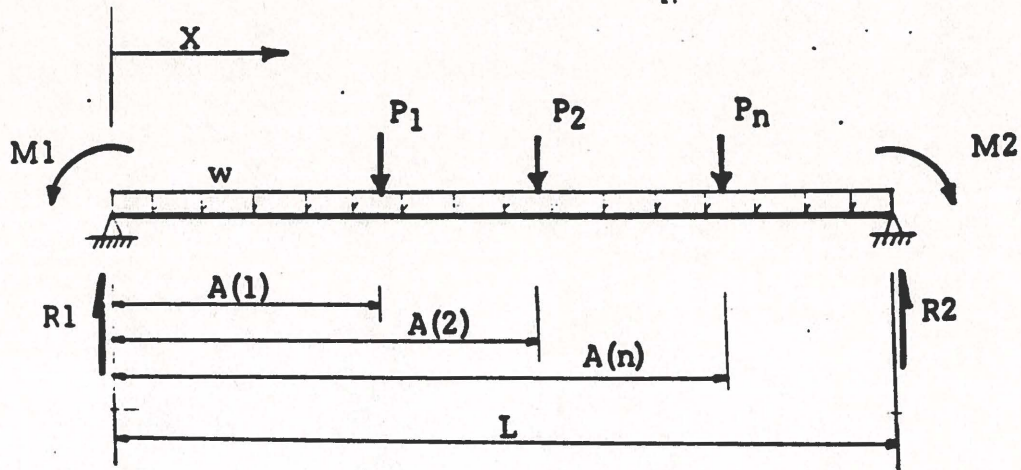
INPUT

Point loads and locations  
Span length  
End moments  
Uniform load  
Location of desired analysis

OUTPUT

Reactions  
Shear at X  
Moment at X

## STRUCTURAL ANALYSIS



C.P. - 25

Data:

Uniform continuous load ( $w$ )	=	1.3 k/ft.
Number of point loads ( $N$ )	=	3
Span length ( $L$ )	=	40 ft.
Applied moment at left ( $M_1$ )	=	100 k-ft.
Applied moment at right ( $M_2$ )	=	100 k-ft.
Location of load 1 $A(1)$	=	10 ft.
Value of load $P(1)$	=	3 k
Location of load 2 $A(2)$	=	20 ft
Value of load $P(2)$	=	3 k
Location of load 3 $A(3)$	=	30 ft.
Value of load $P(3)$	=	3 k
Left Reaction ( $R_1$ )	=	30.5000 k
Right Reaction ( $R_2$ )	=	30.5000 k
Location from left support ( $X$ )	=	10 ft.
Shear at $X$	=	14.5000 k
Moment at $X$	=	140.0000 k-ft.
Location from left support ( $X$ )	=	20 ft.
Shear at $X$	=	-1.5000 k
Moment at $X$	=	220.0000 k-ft.
Location from left support ( $X$ )	=	30 ft.
Shear at $X$	=	-17.5000 k
Moment at $X$	=	140.0000 k-ft.